

Hydraulic Fracture Permeability @model

One of the models of [Hydraulic Fracture Permeability](#) is based on [Cozeny-Karman permeability @model](#):

$(1) \quad k_f = 1014.24 \cdot \text{FZI}^2 \cdot \frac{(\phi_f - \phi_{f0})^3}{(1 - \phi_f + \phi_{f0})^2}$	$(2) \quad \text{FZI} = \frac{1}{\sqrt{F_S} S_{gV} \tau}$
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where

FZI	Flow Zone Indicator	$S_{gV} = \Sigma_e / V_\phi$	surface pore area per unit pore volume	Σ_e	pore surface area
ϕ_f	fracture porosity	F_S	pore shape factor	V_ϕ	pore volume
ϕ_{f0}	porosity cut-off	τ	pore channel tortuosity		

In case of [proppant-filled fracture](#) the [Flow Zone Indicator](#) can be approximated as:

$$(3) \quad \text{FZI} \approx 0.0037 \cdot \frac{d_p}{\tau_p}$$

where

d_p	proppant average grain size
τ_p	fracture pore channel tortuosity

For the fluid-filled [fracture](#) ($\phi_f = 1$) the [fracture permeability](#) has a simple correlation:

$$(4) \quad k_f = \frac{w_f^2}{12}$$

In [Well Testing](#) applications it normally behaves as the infinite-value [fracture permeability](#) due to a high contrast with typical [formation permeability](#).

It can be formally interpreted as the extreme case of finite-conductivity fracture with the following trends:

$(5) \quad \text{FZI} \rightarrow \frac{w_f}{2 \sqrt{F_S}}$	$(6) \quad F_S \rightarrow 253.56 \frac{\phi_{f0}^2}{(1 - \phi_{f0})^3}$
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but this has little practical value.

See Also

[Petroleum Industry](#) / [Upstream](#) / [Well](#) / [Well-Reservoir Contact \(WRC\)](#) / [Hydraulic Fracture](#)