

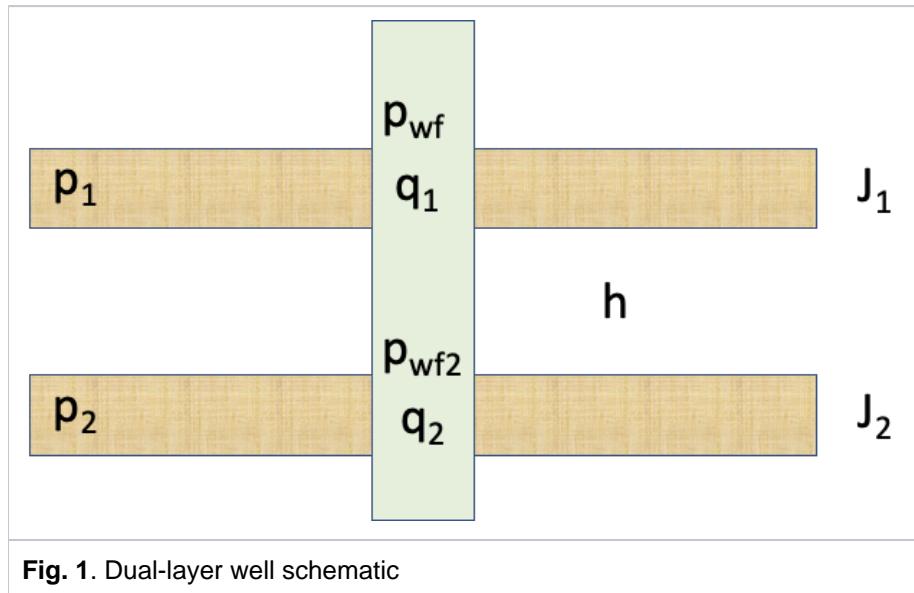
# Dual-layer IPR with dynamic fracture

Consider a water injector with main pay in Reservoir Layer #1 and spontaneous fracture extending down to Reservoir Layer #2 (see **Fig. 1**).

Assume that fracture is not fixed and requires surplus pressure  $\Delta p_f$  to get opened against the rock burden.

When injection bottomhole pressure  $p_{wf}$  is below fracture opening value  $p_{wf} < \Delta p_f$  then water is going to the main pay only (Reservoir Layer #1) and flow radially around the well.

When injection bottomhole pressure  $p_{wf}$  is above fracture opening value  $p_{wf} > \Delta p_f$  then water is going to the fracture and then gets distributed between Reservoir Layer #1 and Reservoir Layer 2



(1)	$q = q_1 + q_2$	(2)	$p_{wf} = p_e + q/J$	(3)	$J = J_1 + J_2$
(4)	$p_e = \Delta p_f + \frac{J_1 \cdot p_1 + J_2 \cdot (p_2 - \delta p_2)}{J_1 + J_2}$				
(5)	$p_e = \frac{J_1 \cdot p_1 + J_2 \cdot p_c}{J_1 + J_2}$				
(6)	$p_c = \left(1 + \frac{J_1}{J_2}\right) \Delta p_f + p_2 - \delta p_2$				

where

Well		
	$q$	total subsurface flowrate of the well

	$J$	total well productivity Index
	$p_e$	apparent formation pressure of dual-layer formation
	$h$	true vertical height between the layers tops
	$\rho$	wellbore fluid density
	$g$	gravity constant
	$\Delta p_f$	fracture opening pressure

### Layer #1

	$p_{wf}$	bottom-hole pressure at Layer #1 top
	$q_1$	total subsurface flowrate of the Layer #1
	$p_1$	formation pressure of the Layer #1
	$J_1$	productivity Index of the Layer #1

### Layer #2

	$p_{wf,2} = p_{wf} + \rho g h$	bottom-hole pressure at Layer #2 top
	$q_2$	total subsurface flowrate of the Layer #2
	$p_2$	formation pressure of the Layer #2
	$J_2$	productivity Index of the Layer #2

$$(7) \quad p_{wf,1} = p_{wf} = \Delta p_f + p_1 + q_1/J_1$$

$$(8) \quad p_{wf,2} = p_{wf} + \delta p_2 = \Delta p_f + p_2 + q_2/J_2$$

This leads to

$$(9) \quad q_1 = J_1 \cdot (p_{wf} - p_1 - \Delta p_f)$$

$$(10) \quad q_2 = J_2 \cdot (p_{wf,2} - p_2 - \Delta p_f) = J_2 \cdot (p_{wf} - (p_2 + \Delta p_f - \delta p_2))$$

and

$$(11) \quad q = q_1 + q_2 = q_1 = J_1 \cdot (p_{wf} - (p_1 + \Delta p_f)) + J_2 \cdot (p_{wf} - (p_2 - \delta p_2 + \Delta p_f))$$

$$(12) \quad q = (J_1 + J_2) \cdot p_{wf} - J_1 \cdot (p_1 + \Delta p_f) + J_2 \cdot ((p_2 - \delta p_2 + \Delta p_f))$$

or

$$(13) \quad q = J \cdot (p_{wf} - p_e), \text{ where } J = J_1 + J_2 \text{ and } p_e = J^{-1} \cdot (J_1 \cdot (p_1 + \Delta p_f) + J_2 \cdot (p_2 - \delta p_2 + \Delta p_f))$$

or

$$(14) \quad p_e = \Delta p_f + J^{-1} \cdot (J_1 \cdot p_1 + J_2 \cdot (p_2 - \delta p_2))$$

## See Also

Petroleum Industry / Upstream / Production / Subsurface Production / Subsurface E&P Disciplines / Field Study & Modelling / Production Analysis / Productivity Diagnostics

[ Production Technology / Well Flow Performance ]

[ Formation pressure (Pe) ] [ Multi-layer IPR ]