

# Water Injection Wellbore Pressure Profile @model

## Motivation

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The stabilized water injection profile satisfies the assumptions of the [Pressure Profile in Incompressible Stationary Quasi-Isothermal Isoviscous Pipe Flow @model](#).

For the stabilized flow the wellbore pressure profile is constant and wellbore temperature profile is changing very slowly.

This allows solving the pressure-temperature problem iteratively:

1. Iterations
  - [Water Injection Wellbore Temperature Profile @model](#)
  - [Water Injection Wellbore Pressure Profile @model](#)
2. Iteration
  - [Water Injection Wellbore Temperature Profile @model](#)
  - [Water Injection Wellbore Pressure Profile @model](#)
3. Iteration ...

## Outputs

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$p(l)$	<a href="#">Pressure distribution along the pipe</a>
$q(l)$	<a href="#">Flowrate distribution along the pipe</a>
$u(l)$	<a href="#">Flow velocity distribution along the pipe</a>

## Inputs

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$T_s$	Intake temperature	$T(l)$	Along-pipe <a href="#">temperature profile</a>
$p_s$	Intake pressure	$\rho(T, p)$	<a href="#">Fluid density</a>
$q_s$	Intake <a href="#">flowrate</a>	$\mu(T, p)$	<a href="#">Fluid viscosity</a>
$z(l)$	<a href="#">Pipeline trajectory TVDss</a>	$d$	Flow <a href="#">pipe diameter</a> (tubing or casing depending on where flow occurs)
$\theta(l)$	<a href="#">Pipeline trajectory inclination</a> , $\cos \theta(l) = \frac{dz}{dl}$	$\epsilon$	Inner pipe wall <a href="#">roughness</a>

## Assumptions

Stationary flow	Homogenous flow	Isothermal or Quasi-isothermal conditions
Incompressible fluid $\rho(T, p) = \rho_s = \text{const}$	Isoviscous flow $\mu(T, p) = \mu_s = \text{const}$	Constant cross-section pipe area $A$ along hole

## Equations

Pressure profile	Pressure gradient profile	Fluid velocity	Fluid rate
(1) $p(l) = p_s + \rho_s g z(l) - \frac{\rho_s q_s^2}{2A^2 d} f_s l$	(2) $\frac{dp}{dl} = \rho_s g \cos \theta(l) - \frac{\rho_s q_s^2}{2A^2 d} f_s$	(3) $q(l) = q_s = \text{const}$	(4) $u(l) = u_s = \frac{q_s}{A} = \text{const}$

where

$f_s = f(\text{Re}, \epsilon)$	Darcy friction factor (see <a href="#">Darcy friction factor in water producing/injecting wells @model</a> ) at intake point
$\text{Re}_s = \frac{4\rho_s q_s}{\pi d} \frac{1}{\mu_s}$	Reynolds number at intake point
$A = 0.25 \pi d^2$	flow pipe cross-section area (tubing or casing depending on where flow occurs)

## See Also

[Petroleum Industry / Upstream / Subsurface E&P Disciplines / Production Technology / Well Flow Performance / Lift Curves \(LC\) / Water Injection Wellbore Profile @model](#)

[ [Pressure Profile in Incompressible Stationary Quasi-Isothermal Isoviscous Pipe Flow @model](#) ] [ [Darcy friction factor in water producing/injecting wells @model](#) ]

[ [Water Injection Wellbore Temperature Profile @model](#) ]