

Watercut Fractional Flow @model

A **proxy model** of **watercut** Y_w in producing well with **reservoir saturation** $s = \{s_w, s_o, s_g\}$ and reservoir pressure p_e :

$$(1) \quad Y_{wm} = \frac{1 - \epsilon_g}{1 + \frac{M_{ro}}{M_{rw}} \cdot \frac{B_w}{B_o}} \quad (2) \quad \epsilon_g = \frac{A}{q_t} \cdot M_{ro} \cdot \left[\frac{\partial P_c}{\partial r} + (\rho_w - \rho_o) \cdot g \cdot \sin \alpha \right]$$

where

$B_w(p_e)$	Water formation volume factor	$B_o(p_e)$	Oil formation volume factor	s	Reservoir saturation $\{s_w, s_o, s_g\}$
$M_{rw}(s)$	Relative water mobility	$M_{ro}(s)$	Relative oil mobility	p_e	Current formation pressure
ρ_w	Water density	ρ_o	Oil density	g	Standard gravity constant
q_t	Total sandface flowrate	A	Cross-sectional flow area	α	Deviation of flow from horizontal plane
$P_c(s)$	capillary pressure				

If capillary effects are not high $P_c \rightarrow 0$ or saturation does not vary along the streamline substantially $\frac{\partial s_w}{\partial r} \rightarrow 0$, then $\frac{\partial P_c}{\partial r} = \dot{P}_c \cdot \frac{\partial s_w}{\partial r} \approx 0$.

If flow is close to horizontal $\sin \alpha \rightarrow 0$ then gravity effects are vanishing too: $(\rho_w - \rho_o) \cdot g \cdot \sin \alpha \approx 0$.

In these cases (1) simplifies to:

$$(3) \quad Y_{wm} = \frac{1}{1 + \frac{M_{ro}}{M_{rw}} \cdot \frac{B_w}{B_o}} = \frac{1}{1 + \frac{k_{ro}}{k_{rw}} \cdot \frac{\mu_w}{\mu_o} \cdot \frac{B_w}{B_o}}$$

The models (1) and (3) can also be used in **production analysis** assuming homogeneous reservoir **water saturation** s_w :

$$(4) \quad s_w(t) = s_{wi} + (1 - s_{wi}) \cdot E_{Dow}(t) = s_{wi} + (1 - s_{wi}) \cdot RFO(t)/E_S$$

where

$RFO = \frac{Q_o^\dagger}{V_{STOIIP}}$	current oil recover factor
$Q_o^\dagger$	cumulative oil production
V_{STOIIP}	STOIIP
E_S	sweep efficiency
s_{wi}	initial water saturation
s_{orw}	residual oil saturation to water sweep

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