

Wellbore Temperature Profile @model

Motivation

One of the key tasks of in [Pipe Flow Dynamics](#) is to predict the along-hole [temperature](#) distribution during the [stationary fluid transport](#).

In many practical cases the [temperature](#) distribution for the [stationary fluid flow](#) can be approximated by [homogenous fluid flow](#) model.

[Pipeline Flow Temperature Model](#) is addressing this problem with account of the varying [pipeline trajectory](#), [pipeline](#) schematic and [heat transfer](#) with surroundings around [pipeline](#).

Outputs

$T(t, l)$	along-pipe temperature distribution and evolution in time
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Inputs

$\mathbf{r}(l)$	pipeline trajectory , $\mathbf{r} = \mathbf{r}(l) = \{x(l), y(l), z(l)\}$	$\rho(T, p)$	fluid density
$A(l)$	pipeline cross-section area	$\mu(T, p)$	fluid viscosity
$T_0(t)$	inflow temperature	$T_{e0}(l)$	initial temperature of the surroundings around the pipeline
p_0	inflow pressure	$c_p(l)$	specific heat capacity of the surroundings around pipeline
q_0	inflow rate	$\lambda_e(l)$	thermal conductivity of the surroundings around pipeline
$U(l)$	heat transfer coefficient based on pipeline schematic		

Physical Model

Stationary flow	Homogenous flow	Axial symmetry around the pipe
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Mathematical Model

Heat transfer in wellbore due to convection and conduction along the wellbore flow	Heat transfer in rocks around the wellbore due to conduction
(1) $\rho c \frac{\partial T}{\partial t} = \frac{d}{dl} \left(\lambda \frac{dT}{dl} \right) - \rho c v \frac{dT}{dl} + \frac{2\lambda}{\lambda_e} \cdot \frac{r_f}{r_w^2} \cdot U \cdot [T_e(t, l, r_w) - T]$	(2) $\rho_e c_e \frac{\partial T_e}{\partial t} = \nabla(\lambda_e \nabla T_e)$
(3) $T(t = 0, l) = T_{e0}(l)$	(4) $T_e(t = 0, l, r) = T_{e0}(l)$
(5) $T(t, l = 0) = T_0(t)$	(6) $T_e(t, l, r \rightarrow \infty) = T_{e0}(l)$
(7) $T(t, l = l_{max}) = T_{e0}(l_{max})$	(8) $T_e(t, 0, r) = T_s(t)$
	(9) $T_e(t, l_{max}, r) = T_{e0}(l_{max})$
Heat exchange between wellbore fluid and rocks around the wellbore	
(10)	$2\pi \lambda_e r_w \frac{\partial T_e}{\partial r} \Big _{r=r_w} = 2\pi r_f U \cdot \left(T_e \Big _{r=r_w} - T \right)$

(see [Derivation of Stationary Isothermal Homogenous Pipe Flow Pressure Profile @model](#))

Proxy Models

Linear superposition of [Homogenous Pipe Flow Temperature Profile @model](#) and [Linear Semiplane Temperature Profile @model](#)

See also

[Physics](#) / [Fluid Dynamics](#) / [Pipe Flow Dynamics](#) / [Pipe Flow Simulation](#)

[[Heat Transfer](#)] [[Heat Transfer Coefficient \(HTC\)](#)] [[Heat Transfer Coefficient @model](#)]

[[Wellbore Injection Homogeneous Flow @model](#)] [[Temperature Profile in Wellbore Injection Homogeneous Flow Analytical @model](#)]

[[Wellbore Homogeneous Flow Production @model](#)] [[Temperature Profile in Wellbore Production Homogeneous Flow Analytical @model](#)]

References

https://en.wikipedia.org/wiki/Darcy_friction_factor_formulae

https://neutrium.net/fluid_flow/pressure-loss-in-pipe/