

Horner Test

Specific schematic of **Pressure Test** consisting of long-term shut-in, followed by **FLOWING** survey (**Drawdown** / **Injection**) then followed by **SHUT-IN** survey(**Build-up** / **Fall-off**) (see **Fig. 1**).

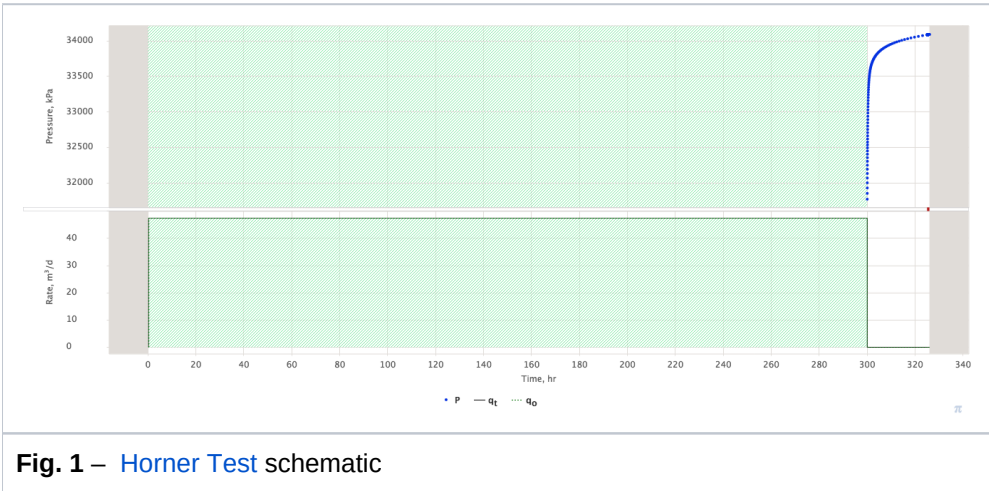


Fig. 1 – **Horner Test** schematic

The interpretation of **Horner Test** can be performed by conventional **pressure diffusion models** fitting.

But historically it was given a specific popularity due to computational simplifications from using the **Superposition Time** concept, particularly when the following conditions hold true:

Condition 1	Both FLOWING T and SHUT-IN Δt periods reach radial flow regime: $T > t_{IARF}$, $\Delta t > t_{IARF}$
Condition 2	The total duration of FLOWING and SHUT-IN does not reach the boundary $T + \Delta t < t_e$

In this case the **pressure diffusion** during the **SHUT-IN** period can be simulated as:

(1)
$$p_{wf}(\Delta t) = p_e - \frac{q_i}{4\pi\sigma} \ln\left(1 + \frac{T}{\Delta t}\right)$$

The equation (1) shows that pressure during this period of time is not dependent on skin-factor S and pressure diffusivity χ but provide an easy linear way to assess formation pressure p_e and formation transmissibility σ .

The benefits of this interpretation method is that:

- it provides the robust straightforward estimation of formation pressure p_e and formation transmissibility σ
- it does not require the knowledge of pressure diffusivity χ
- it does not depend on diffusion model specifics as soon as **IARF** is developed during the test and the outer boundary did not affect the pressure

It should be mentioned that in modern **Pressure Transient Analysis** the above **Condition 1** and **Condition 2** are not required and one can use the powerful arsenal of modern softwares to fit the pressure readings with **pressure diffusion models**.

See Also

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