

# Slightly compressible Material Balance Pressure @model

Approximation of [Material Balance Pressure @model](#) for [slightly compressibility flow](#):

|     |                                                                                                                                                                                                                               |
|-----|-------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|
| (1) | $p(t) = p_i + \frac{\Delta Q(t)}{V_\phi \cdot c_t}$                                                                                                                                                                           |
| (2) | $\Delta Q = -\frac{B_o - R_s B_g}{1 - R_s R_v} \cdot Q_O^\uparrow + \frac{B_g - R_v B_o}{1 - R_s R_v} \cdot (Q_G^\downarrow - Q_G^\uparrow + Q_{GCAP}^\downarrow) + B_w (Q_W^\downarrow - Q_W^\uparrow + Q_{WAQ}^\downarrow)$ |

where

|                                                       |                                                                             |
|-------------------------------------------------------|-----------------------------------------------------------------------------|
| $\Delta Q(t)$                                         | Cumulative Voidage Replacement Balance (CVRB) over time $t$                 |
| $V_\phi = V \cdot \phi_i$                             | initial drainage volume of the main pay (excluding the aquifer and gas cap) |
| $\phi_i = \phi(p_i)$                                  | initial porosity                                                            |
| $c_t = c_\phi + c_o s_{oi} + c_g s_{gi} + c_w s_{wi}$ | total compressibility                                                       |
| $c_\phi$                                              | pore compressibility                                                        |
| $s_{wi}$                                              | initial water saturation                                                    |
| $s_{gi}$                                              | initial gas saturation                                                      |
| $s_{oi}$                                              | initial oil saturation: $s_{oi} = 1 - s_{wi} - s_{gi}$                      |
| $c_o, c_g, c_w$                                       | fluid compressibility of water phase, oil phase and gas phase               |

The equations (1) and (2) are often used in express assessment of thief water production share  $\Omega_W^\uparrow = Q_{W,true}^\uparrow / Q_W^\uparrow$  and thief water injection share  $\Omega_W^\downarrow = Q_{W,true}^\downarrow / Q_W^\downarrow$ :

|     |                                                                                                            |     |                                                                                                                                                   |     |                                                                                                                                                          |
|-----|------------------------------------------------------------------------------------------------------------|-----|---------------------------------------------------------------------------------------------------------------------------------------------------|-----|----------------------------------------------------------------------------------------------------------------------------------------------------------|
| (3) | $p_i - p(t) = \alpha \cdot Q_O^\uparrow(t) + \beta \cdot Q_W^\uparrow(t) - \gamma \cdot Q_W^\downarrow(t)$ | (4) | $\alpha > 0, \quad \beta > 0, \quad \gamma > 0$                                                                                                   |     |                                                                                                                                                          |
| (5) | $V_\phi = \frac{1}{\alpha \cdot c_t} \cdot \frac{B_o - R_s B_g}{1 - R_s R_v}$                              | (6) | $\Omega_W^\uparrow = \frac{Q_{W,true}^\uparrow}{Q_W^\uparrow} = \frac{\beta}{\alpha} \cdot \frac{1}{B_w} \cdot \frac{B_o - R_s B_g}{1 - R_s R_v}$ | (7) | $\Omega_W^\downarrow = \frac{Q_{W,true}^\downarrow}{Q_W^\downarrow} = \frac{\gamma}{\alpha} \cdot \frac{1}{B_w} \cdot \frac{B_o - R_s B_g}{1 - R_s R_v}$ |

## See Also

[Petroleum Industry / Upstream / Production / Subsurface Production / Field Study & Modelling / Production Analysis / Material Balance Analysis \(MatBal\) / Material Balance Pressure @model](#)

[ [Derivation of Slightly compressible Material Balance Pressure @model](#) ]

[ [Capacitance-Resistivity Model \(CRM\) @model](#) ]